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# Production characteristics of reactive oxygen/nitrogen species in water using atmospheric pressure discharge plasmas

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A pulsed discharge, a DC corona discharge, and a plasma jet are separately generated above a water surface, and reactive oxygen species and reactive nitrogen species (ROS/RNS) in the water are investigated. ROS/RNS in water after the sparging of the off-gas of a packed-bed dielectric barrier discharge (PB-DBD) are also investigated.  $H_2O_2$ ,  $NO_2^-$ , and  $NO_3^-$  are detected after plasma exposure and only  $NO_3^-$  after off-gas sparging. Short-lifetime species in plasma are found to play an important role in  $H_2O_2$  and  $NO_2^-$  production and long-lifetime species in  $NO_3^-$  production.  $NO_x$  may inhibit  $H_2O_2$  production through OH consumption to produce  $HNO_2$  and  $HNO_3$ .  $O_3$  does not contribute to ROS/RNS production. The pulsed plasma exposure is found to be effective for the production of  $H_2O_2$  and  $NO_2^-$ , and the off-gas sparging of the PB-DBD for the production of  $NO_3^-$ . © 2016 The Japan Society of Applied Physics

# <sup>21</sup> 1. Introduction

<sup>23</sup> In recent years, the study of plasma in contact with water has <sup>24</sup> gained increasing attention and the water is known as plasma-<sup>25</sup> treated water (PTW; also called plasma-activated medium, <sup>26</sup> plasma-activated water, and so on). PTW is produced by <sup>27</sup> various types of discharge plasma such as gliding arc,<sup>1–3)</sup> <sup>28</sup> plasma jet,<sup>4–6)</sup> and dielectric barrier discharge.<sup>7,8)</sup> In general, <sup>29</sup> many kinds of species, such as radicals, ions, and ozone (O<sub>3</sub>), <sup>30</sup> are produced in plasma, and some of the species in the <sup>31</sup> plasma in contact with water act as precursors of reactive <sup>32</sup> oxygen species and reactive nitrogen species (ROS/RNS) in <sup>33</sup> water.

PTW containing the ROS/RNS is applied to various fields 34  $_{35}$  such as disinfection,  $^{1,3-5,7,8)}$  agriculture,  $^{2,9)}$  and plasma <sup>36</sup> medicine.<sup>6)</sup> Several groups suggested that hydrogen peroxide 37 (H<sub>2</sub>O<sub>2</sub>), peroxynitrous acid (HOONO), nitrite (NO<sub>2</sub><sup>-</sup>), nitric 38 acid (HNO<sub>3</sub>), and/or synergistic effects between these <sup>39</sup> species in water play a key role in bacterial inactivation, 40 plant germination and growth, and chemical and biological <sup>41</sup> effects. Naïtali et al.<sup>1)</sup> reported that PTW and acidified water, <sup>42</sup> containing 0.01 mmol/L  $H_2O_2$ , 1.6 mmol/L  $NO_2^-$ , and  $_{43}$  0.13 mmol/L nitrate (NO<sub>3</sub><sup>-</sup>), show a lethal effect on *Hafnia* <sup>44</sup> alvei. Kim et al.<sup>3)</sup> found that PTW containing 2.94 mmol/L <sup>45</sup> H<sub>2</sub>O<sub>2</sub> contributes to 5-log reduction for *Escherichia coli*. <sup>46</sup> Takaki<sup>9)</sup> reported that water containing 0.12 mmol/L NO<sub>3</sub><sup>-</sup> 47 contributes to the improvement of the growth rate of Brassica <sup>48</sup> *rapa* var. *perviridis*. Furthermore, Matsui et al.<sup>10)</sup> also 49 suggested that long-lifetime neutral particles in the gas 50 phase, such as  $O_3$ ,  $H_2O_2$ , and HNO<sub>3</sub>, and synergistic effects 51 between these species play a key role in the disinfection of 52 Geobacillus stearothermophilus spores. To utilize the PTW <sup>53</sup> effectively and efficiently, it is important to control the ROS/ 54 RNS concentration and to clarify the interaction between 55 species in plasma and ROS/RNS in water as well as to <sup>56</sup> investigate efficacy in the application fields, since PTW with 57 a wide-ranging ROS/RNS concentration is used for the 58 investigation of efficacy. Various types of discharge plasma 59 can produce the ROS/RNS; however, few studies have 60 focused on the correlation between the discharge plasma and 61 the ROS/RNS as far as we know.

In this work, we generated a pulsed discharge, a DC <sup>21</sup> corona discharge, an atmospheric pressure plasma jet, and a <sup>22</sup> packed-bed dielectric barrier discharge (PB-DBD) as a <sup>23</sup> plasma source to produce ROS/RNS in water. We exposed <sup>24</sup> deionized water to the pulsed discharge, DC corona dis-<sup>26</sup> charge, or plasma jet. We also sparged the off-gas of the <sup>26</sup> PB-DBD into deionized water. Then, we investigated the <sup>27</sup> concentration and production efficiency of the ROS/RNS in <sup>28</sup> the water. <sup>29</sup>

# 2. Experimental procedure

## 2.1 Pulsed discharge

The experimental apparatus for a pulsed discharge is similar 33 to that used in a previous work.<sup>11)</sup> A needle electrode and a <sup>34</sup> water bath electrode were placed in a cylindrical discharge 35 chamber to generate the pulsed discharge. The needle 36 electrode was a stainless-steel nail with a diameter of 37 1.5 mm and a length of 19 mm, the water bath electrode 38 was made of stainless steel with an inner diameter of 39 119 mm, a depth of 12 mm, and a capacity of 0.13 L, and the 40 cylindrical chamber was made of acrylic resin with an inner 41 diameter of 140 mm, a height of 100 mm, and a capacity of 42 1.54 L. Deionized water of 100 mL was poured into the water 43 bath electrode, and the distance between the tip of the needle 44 electrode and the water surface was fixed at 4 mm. Ar, N<sub>2</sub>, 45 O<sub>2</sub>, or a gas mixture of Ar/O<sub>2</sub>, N<sub>2</sub>/O<sub>2</sub>, or Ar/N<sub>2</sub> was used <sup>46</sup> as a background (BG) gas, and fed into the chamber at a 47 constant flow rate of 5 L/min. The gas mixture ratios were 48  $Ar/O_2$ ,  $N_2/O_2$ , and  $Ar/N_2 = 80/20$ , 60/40, 40/60, and 49 20/80%. 50

A pulsed high voltage with a pulse width of 500 ns <sup>51</sup> generated by a Blumlein generator, which has two coaxial <sup>52</sup> transmission lines (Fujikura 5D-2V) with a length of 50 m <sup>53</sup> and a capacitance of 5 nF, was applied to the needle electrode <sup>54</sup> to generate the pulsed discharge above the water surface. The <sup>55</sup> coaxial transmission lines were charged to a negative voltage <sup>56</sup> of 14.14 kV, and the pulse repetition rate was 20 pps (pulse <sup>57</sup> per second). The applied voltage was measured using a high- <sup>58</sup> voltage probe (Iwatsu Test Instruments HV-P30) and the <sup>59</sup> discharge current was obtained by measuring the voltage <sup>60</sup> drop across a non-inductive resistor connected in series <sup>61</sup>

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<sup>17</sup> Fig. 1. (Color online) Schematic diagram of experimental apparatus for
 <sup>18</sup> plasma jet.

<sup>21</sup> between the bath electrode and the ground. The input power
<sup>22</sup> was calculated by multiplying the applied voltage and
<sup>23</sup> discharge current, and the input energy was obtained from
<sup>24</sup> the time integration of the input energy. Water samples of
<sup>25</sup> 1.2 mL were taken after plasma exposure and analyzed using
<sup>26</sup> a high-performance liquid chromatograph (HPLC; Shimadzu
<sup>27</sup> Prominence) equipped with an ion chromatography column
<sup>28</sup> (Shodex IC NI-424) in combination with an autosampler. The
<sup>29</sup> eluent of the HPLC was a mixed solution of 3 mmol/L acetic
<sup>30</sup> acid and 1.9 mmol/L potassium hydroxide, and the wave<sup>31</sup> length of the absorbance detector was fixed at 220 nm.

## 33 2.2 Corona discharge

34 The experimental apparatus for a corona discharge is similar <sup>35</sup> to that used in a previous work.<sup>12)</sup> A comb-shaped electrode <sup>36</sup> and a plastic container were placed in an acrylic discharge 37 chamber with a length of 140 mm, a width of 260 mm, and a <sup>38</sup> height of 100 mm. The comb-shaped electrode consisted of <sup>39</sup> four clusters, each of which has 26  $(13 \times 2)$  combs, with a 40 width of 1.6 mm and a length of 15 mm, placed at intervals 41 of 4 mm. Deionized water of 100 mL was poured into the 42 container, and the distance between the tip of the electrode 43 and the water surface was fixed at 15 mm. An aluminum foil 44 was immersed into the water and earthed. A gas mixture of 45  $N_2/O_2$  or  $Ar/O_2$  was used as a BG gas and fed into the 46 chamber at a constant flow rate of 2L/min. The BG gas 47 mixture ratios were  $Ar/O_2 = 80/20, 60/40, and 40/60\%$ , and <sup>48</sup>  $N_2/O_2 = 60/40$  and 40/60%. A positive DC high voltage 49 of 14.7–15.4 kV was applied to the electrode to generate a <sup>50</sup> corona discharge between the electrode and the water surface, <sup>51</sup> with an input power of 6 W. The input energy was obtained <sup>52</sup> from the time integration of the input power. Water samples of <sup>53</sup> 1.2 mL were analyzed using the HPLC after plasma exposure. 54

### 55 2.3 Plasma jet

Figure 1 shows a schematic diagram of the experimental apparatus for the plasma jet. The atmospheric pressure plasma jet reactor consisted of a T-shaped glass tube, a copper tube, and an aluminum sheet. The copper tube was inserted into an end of the main tube of the T-shaped glass tube, and the aluminum sheet was bound around the main 28

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tube and earthed. The gap length between the copper tube 1 and the aluminum sheet was fixed at 10 mm. An Ar or He gas 2 was fed into the main tube through the copper tube at a 3 constant flow rate of 10 or 5 L/min, respectively. A gas 4 mixture of N<sub>2</sub>/O<sub>2</sub>, the mixture ratio of which is N<sub>2</sub>/O<sub>2</sub> = 5 100/0, 80/20, 60/40, 40/60, 20/80, and 0/100%, was mixed 6 into the plasma jet from the side tube of the T-shaped glass 7 tube at a constant flow rate of 0.1 L/min.

An AC high voltage of 6.0–7.0 kV amplitude generated by 9 a neon-sign transformer (Kodera Electronics CR-N16) was 10 applied to the copper tube to generate the plasma jet. The 11 input power was calculated by the Lissajous figure method,  $^{13}$  12 and the input energy was obtained from the time integration 13 of the input power. The applied voltage was measured using 14 a high-voltage probe (Tektronix P6015A), and the charge 15 amount was obtained by measuring the voltage drop across a 16 ceramic capacitor with a capacitance of 10 nF, connected in 17 series between the aluminum sheet and the ground. The 18 voltage drop was measured using a high-voltage differential 19 probe (GW Instek GDP-100). Deionized water of 200 mL 20 was poured into a beaker placed below the plasma jet. The 21 distance between the water surface and the outlet end of the 22 main tube was fixed at 65 or 15 mm. The Ar gas flow rate was 23 fixed at 5 L/min when the distance was fixed at 15 mm. The 24 water was exposed to the plasma jet, and then water samples 25 of 1.2 mL were taken and analyzed using the HPLC after 26 plasma exposure. 27

# 2.4 Packed-bed dielectric barrier discharge

The experimental apparatus for a packed-bed dielectric barrier <sup>30</sup> discharge (PB-DBD) is similar to that used in a previous <sup>31</sup> work.<sup>14)</sup> A PB-DBD reactor consisted of a glass tube filled <sup>32</sup> with soda-lime glass balls, an inner rod electrode, and an outer <sup>33</sup> mesh electrode. The diameters of the glass tube, glass balls, <sup>34</sup> and rod electrode were 22, 3.0, and 2.0 mm, respectively. Ar, <sup>35</sup> N<sub>2</sub>, O<sub>2</sub>, or a gas mixture of Ar/O<sub>2</sub>, N<sub>2</sub>/O<sub>2</sub>, or Ar/N<sub>2</sub> was <sup>36</sup> used as a BG gas and fed into the reactor at a constant flow <sup>37</sup> rate of 2 L/min. The gas mixture ratios were Ar/O<sub>2</sub>, N<sub>2</sub>/O<sub>2</sub>, <sup>38</sup> and Ar/N<sub>2</sub> = 80/20, 60/40, 40/60, and 20/80%.

A sinusoidal high voltage of 5.7–12.0 kV amplitude <sup>40</sup> generated by the neon-sign transformer was applied between <sup>41</sup> electrodes to generate the PB-DBD. The input energy was <sup>42</sup> obtained from the time integration of input power calculated <sup>43</sup> by the Lissajous figure method. The off-gas from the reactor <sup>44</sup> was introduced through a Teflon tube with a length of 60 cm <sup>45</sup> and an inner diameter of 3.96 mm and sparged into deionized <sup>46</sup> water of 100 mL in a flask. Water samples of 1.2 mL were <sup>47</sup> taken and analyzed using the HPLC after off-gas sparging. <sup>48</sup> Furthermore, the PB-DBD off-gas was analyzed using a <sup>49</sup> Fourier transform infrared spectrophotometer (JASCO FT/ <sup>50</sup> IR-4200) equipped with a gas cell (Infrared Analysis 10-PA), <sup>51</sup> which has an optical path length of 10 m.

# 3. Results and discussion

In HPLC analysis,  $H_2O_2$ ,  $NO_2^-$ , and  $NO_3^-$  were detected in <sup>55</sup> the sampled water. Figure 2 shows the  $H_2O_2$  concentrations <sup>56</sup> in the sampled water as functions of specific energy, which is <sup>57</sup> defined as the input energy per unit volume of water.  $H_2O_2$  <sup>58</sup> was produced in the cases of pulsed discharge, corona <sup>59</sup> discharge, and plasma jet, but not in the case of PB-DBD off-<sup>60</sup> gas sparging; therefore, short-lifetime active and/or energetic <sup>61</sup>

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Fig. 2. (Color online)  $H_2O_2$  concentrations in sampled water as functions of specific energy: (a) pulsed discharge, (b) corona discharge, (c) plasma jet, and (d) PB-DBD.

<sup>34</sup> species in the plasma in contact with water probably <sup>35</sup> contribute to  $H_2O_2$  production. When water is exposed to <sup>36</sup> plasma, vaporized water molecules can be dissociated as <sup>37</sup> follows:<sup>15–17</sup>

<sup>38</sup>  $H_2O + e \rightarrow OH + H + e,$  (1)

$$H_2O + e \to H_2O^+ + 2e, \qquad (2)$$

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$$H_2O^+ + H_2O \to H_3O^+ + OH.$$
 (3)

 $^{\mbox{\tiny 42}}$  Then,  $H_2O_2$  can be produced from OH radicals represented  $^{\mbox{\tiny 43}}$  as  $^{18,19)}$ 

<sup>44</sup> OH + OH 
$$\rightarrow$$
 H<sub>2</sub>O<sub>2</sub> (k = 1.5 × 10<sup>-11</sup> cm<sup>3</sup>·mol<sup>-1</sup>·s<sup>-1</sup>), (4)

<sup>46</sup> where *k* is the rate constant. Although water vapor is <sup>47</sup> contained within the concentration of 20 ppm as impurities in <sup>48</sup> the BG gas of the PB-DBD, the concentration of OH radicals <sup>49</sup> can be quite small, so that  $H_2O_2$  produced by the reaction <sup>50</sup> shown by Eq. (4) is negligible.

<sup>51</sup>  $H_2O_2$  concentrations in the pulsed discharge monotonically <sup>52</sup> increased with the specific energy, while the amount of  $H_2O_2$ <sup>53</sup> in the BG gas containing N<sub>2</sub> was found to be smaller than that <sup>54</sup> in the other BG gas. This may be due to the inhibition of <sup>55</sup>  $H_2O_2$  production by species containing N atom(s). The  $H_2O_2$ <sup>56</sup> production efficiency of 31.2 µmol/kJ at a maximum was <sup>57</sup> obtained when an Ar/O<sub>2</sub> mixture was used. The  $H_2O_2$ <sup>58</sup> concentrations in the corona discharge tended to increase <sup>59</sup> with Ar or N<sub>2</sub> content in the mixture gas, and the maximum <sup>60</sup>  $H_2O_2$  production efficiency of 7.6 µmol/kJ was obtained in <sup>61</sup> Ar/O<sub>2</sub> = 80/20%. When the plasma jet was used, the amount of  $H_2O_2$  was small and slightly increased with the shortening <sup>34</sup> of the distance between the plasma and the water surface. The <sup>35</sup>  $H_2O_2$  production efficiency in Ar without the  $N_2/O_2$  mixture <sup>36</sup> was  $1.7 \,\mu$ mol/kJ, which is significantly lower than that in <sup>37</sup> pulsed discharge. Van Gils et al.<sup>5)</sup> investigated the  $H_2O_2$  <sup>38</sup> concentrations in water exposed to an Ar plasma jet, and <sup>39</sup> reported that the  $H_2O_2$  production efficiency was  $0.7 \,\mu$ mol/kJ <sup>40</sup> at a maximum. This value differs slightly from the efficiency <sup>41</sup> of this work, so that pulsed discharge may be suitable for <sup>42</sup> highly efficient  $H_2O_2$  production. <sup>43</sup>

Figure 3 shows the  $NO_2^-$  concentrations in the sampled <sup>44</sup> water as functions of specific energy.  $NO_2^-$  was produced by <sup>45</sup> exposure to the pulsed discharge, corona discharge, and <sup>46</sup> plasma jet when the BG gas contained N<sub>2</sub>, but not by the <sup>47</sup> sparging of the PB-DBD off-gas; therefore, short-lifetime <sup>48</sup> active and/or energetic species in the plasma in contact with <sup>49</sup> water probably contribute to  $NO_2^-$  production. Furthermore, <sup>50</sup> the  $NO_2^-$  concentration in the pulsed discharge was found <sup>51</sup> to increase and then decrease with the increase in specific <sup>52</sup> energy. When water is exposed to plasma in the BG gas <sup>53</sup> containing N<sub>2</sub>, the following reactions<sup>20)</sup> can occur:

$$N_2 + e(fast) \rightarrow 2N + e(slow), \qquad (5)^{56}$$

$$N + OH \rightarrow NO + H$$

$$(k = 4.9 \times 10^{-11} \,\mathrm{cm}^3 \cdot \mathrm{mol}^{-1} \cdot \mathrm{s}^{-1}),$$
 (6) 58

$$NO + OH + M \rightarrow HNO_2 + M$$

$$(k = 7.4 \times 10^{-31} \,\mathrm{cm}^{6} \cdot \mathrm{mol}^{-2} \cdot \mathrm{s}^{-1}),$$
 (7)

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Fig. 3. (Color online) NO<sub>2</sub><sup>-</sup> concentrations in sampled water as functions of specific energy: (a) pulsed discharge, (b) corona discharge, (c) plasma jet, and  $_{37}$  (d) PB-DBD.

<sup>35</sup> where M is the third body. Then, HNO<sub>2</sub> dissolves in water <sup>36</sup> and dissociates into NO<sub>2</sub><sup>-</sup> and H<sup>+</sup> in acid-base equilibrium <sup>37</sup> ( $pK_a = 3.3$ ) represented by<sup>5,21</sup>)

$$HNO_2 \rightleftharpoons NO_2^- + H^+. \tag{8}$$

<sup>40</sup> Furthermore, HNO<sub>2</sub> reacts with  $H_2O_2$  to form HOONO <sup>41</sup> by<sup>5,22)</sup>

<sup>42</sup>  $HNO_2 + H_2O_2 \rightarrow HOONO + H_2O.$  (9)

<sup>44</sup> HOONO is an unstable species and rapidly turns into  $NO_3^-$ <sup>45</sup> and H<sup>+</sup>.<sup>22)</sup>

<sup>46</sup> HOONO 
$$\rightarrow$$
 NO<sub>3</sub><sup>-</sup> + H<sup>+</sup>. (10)

<sup>48</sup> In this work, the pH drop of the water after pulsed discharge <sup>49</sup> exposure was observed, and the pH decreased below 4.0 after <sup>50</sup> 5 min exposure (corresponding to a specific energy of 32 <sup>51</sup> kJ/L) and 3.0 after 30 min exposure (corresponding to a <sup>52</sup> specific energy of 208 kJ/L) in N<sub>2</sub>/O<sub>2</sub> = 80/20%. Therefore, <sup>53</sup> NO<sub>2</sub><sup>-</sup> in the water may be converted into NO<sub>3</sub><sup>-</sup> through the <sup>54</sup> reactions shown by Eqs. (8)–(10), resulting in the drop of <sup>55</sup> the NO<sub>2</sub><sup>-</sup> concentration with the increase in specific energy. <sup>56</sup> NO<sub>2</sub><sup>-</sup> concentrations in the corona discharge and plasma jet <sup>57</sup> showed a tendency to saturate, and this result is also probably <sup>58</sup> due to the drop in the pH of the water. The maximum NO<sub>2</sub><sup>-</sup> <sup>59</sup> production efficiency of 5.0 µmol/kJ was obtained using the <sup>60</sup> pulsed discharge in N<sub>2</sub>/Ar = 20/80% at the specific energy <sup>61</sup> of 25 kJ/L. In the PB-DBD, the BG gas contains water vapor within <sup>35</sup> the concentration of 20 ppm as impurities, and the concentration is six orders of magnitude lower than that of N<sub>2</sub>. OH <sup>37</sup> radicals can be produced from a trace of water vapor, but <sup>38</sup> the concentration of OH radicals can be much lower than that <sup>39</sup> of N atoms produced from N<sub>2</sub> in the PB-DBD; therefore, the <sup>40</sup> reaction shown by Eq. (4) can be negligible and the reactions <sup>41</sup> shown by Eqs. (6) and (7) can occur. However, NO<sub>2</sub><sup>-</sup> was <sup>42</sup> not detected, so that the concentration of NO<sub>2</sub><sup>-</sup> in the water <sup>43</sup> was below the detection limit (20 nmol/L) or NO<sub>2</sub><sup>-</sup> was <sup>44</sup> rapidly converted into other species. <sup>45</sup>

Figure 4 shows the NO<sub>3</sub><sup>-</sup> concentrations in the sampled <sup>46</sup> water as functions of specific energy. When water is exposed <sup>47</sup> to plasma in the BG gas containing N<sub>2</sub>, the following <sup>48</sup> reactions<sup>18,23</sup> may occur in addition to the reactions shown <sup>49</sup> by Eqs. (5)–(7): <sup>50</sup>

$$NO + O + M \rightarrow NO_2 + M$$
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$$(k = 8.9 \times 10^{-32} \,\mathrm{cm}^{6} \cdot \mathrm{mol}^{-2} \cdot \mathrm{s}^{-1}),$$
 (11) 53

$$NO_2 + OH + M \rightarrow HNO_3 + M$$
 <sup>54</sup>

$$(k = 2.6 \times 10^{-30} \,\mathrm{cm}^{6} \cdot \mathrm{mol}^{-2} \cdot \mathrm{s}^{-1}). \tag{12}$$

Then, HNO<sub>3</sub> dissolves in water and completely dissociates <sup>57</sup> into NO<sub>3</sub><sup>-</sup> and H<sup>+</sup>. The reactions shown by Eqs. (8)–(10) <sup>58</sup> also contribute to NO<sub>3</sub><sup>-</sup> production. Furthermore, the pro- <sup>59</sup> duction of HNO<sub>2</sub> and HNO<sub>3</sub> by the reactions shown by <sup>60</sup> Eqs. (7) and (12) causes OH consumption, so that H<sub>2</sub>O<sub>2</sub> <sup>61</sup>

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<sup>30</sup> **Fig. 4.** (Color online)  $NO_3^-$  concentrations in sampled water as functions of specific energy: (a) pulsed discharge, (b) corona discharge, (c) plasma jet, and <sup>30</sup> (d) PB-DBD.

can occur.<sup>28)</sup>

<sup>36</sup> production by the reaction shown by Eq. (4) is inhibited, <sup>37</sup> resulting in the decrease in the  $H_2O_2$  amount in the BG gas <sup>38</sup> containing N<sub>2</sub>.

NO<sub>3</sub><sup>-</sup> was also produced by off-gas sparging. In the PB-39 40 DBD, a trace of OH radicals is produced from water vapor 41 contained in the BG gas as impurities, as described above, so <sup>42</sup> that the reaction shown by Eq. (12) has little contribution to 43 HNO<sub>3</sub> production. Thus, other reactions by long-lifetime <sup>44</sup> species to produce  $NO_3^-$  may occur in off-gas sparging. The <sup>45</sup> NO<sub>3</sub><sup>-</sup> concentrations in the pulsed discharge monotonically  $_{46}$  increased with the specific energy, and the NO<sub>3</sub><sup>-</sup> production 47 efficiency of 5.1 µmol/kJ was obtained at a maximum. In the <sup>48</sup> corona discharge, NO<sub>3</sub><sup>-</sup> tended to increase with Ar or N<sub>2</sub> <sup>49</sup> content in the mixture gas, and the NO<sub>3</sub><sup>-</sup> production 50 efficiency of 8.0 µmol/kJ was obtained. When the plasma  $_{51}$  jet was used, the amount of NO<sub>3</sub><sup>-</sup> was small and slightly 52 increased with N<sub>2</sub> mixing. In the case of off-gas sparging,  $_{53}$  NO<sub>3</sub><sup>-</sup> was produced in the N<sub>2</sub>/O<sub>2</sub> mixture and its amount was found to increase with N2 content. The maximum 54 55 NO<sub>3</sub><sup>-</sup> production efficiency of 11.3 µmol/kJ was obtained in 56 N<sub>2</sub>/O<sub>2</sub> = 80/20%.

Figure 5 shows the absorbance spectra of the PB-DBD off-gas before and after sparging, obtained by infrared be absorption spectroscopy. Absorption peaks corresponding to nitrous oxide (N<sub>2</sub>O; 2224 cm<sup>-1</sup>),<sup>24</sup> dinitrogen pentaoxide (N<sub>2</sub>O<sub>5</sub>; 1247, 1704, and 1745 cm<sup>-1</sup>),<sup>25</sup>) HNO<sub>3</sub> (1312, 1346, and  $1698 \text{ cm}^{-1}$ ,<sup>26)</sup> and O<sub>3</sub> ( $1042 \text{ cm}^{-1}$ )<sup>27)</sup> were detected in <sup>36</sup> the N<sub>2</sub>/O<sub>2</sub> mixture. It was suggested above that a trace of <sup>37</sup> NO<sub>2</sub><sup>-</sup> might be produced in water via the reaction shown <sup>38</sup> by Eq. (7); however, NO<sub>2</sub><sup>-</sup> was not detected. O<sub>3</sub> was <sup>39</sup> observed in the off-gas as shown in Fig. 5 and O<sub>3</sub> can <sup>40</sup>

$$NO_2^- + O_3 \rightarrow NO_3^- + O_2.$$
 (13)<sup>4</sup>

Furthermore, considering that  $NO_2^-$  was not detected, the 45 rate of reaction can be sufficiently high.

dissolve in water; therefore, the reaction shown by Eq. (13) 41

It was described that a trace of HNO<sub>3</sub> is produced via the <sup>47</sup> reaction shown by Eq. (12). In addition, HNO<sub>3</sub> may also be <sup>48</sup> produced by the reaction shown by Eq. (14),<sup>18)</sup> since  $N_2O_5$  <sup>49</sup> and water vapor are contained in the off-gas before sparging, <sup>50</sup> as shown in Fig. 5.

$$N_2O_5 + H_2O \to 2HNO_3.$$
 (14)

The intensities of absorption peaks corresponding to  $N_2O_5$  <sup>54</sup> and HNO<sub>3</sub> were reduced by sparging, while there were little <sup>55</sup> changes in the intensities of absorption peaks corresponding <sup>56</sup> to  $N_2O$  and  $O_3$ . This indicates that HNO<sub>3</sub> in the off-gas <sup>57</sup> dissolves in water and HNO<sub>3</sub> is produced in liquid phase <sup>58</sup> by the reaction shown by Eq. (14), contributing to  $NO_3^-$  <sup>59</sup> production, and that  $N_2O$  and  $O_3$  do not produce ROS/RNS <sup>60</sup> in water.

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#### 4. Conclusions

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We have investigated reactive oxygen species and reactive 19 20 nitrogen species (ROS/RNS) in water, exposed directly to a pulsed discharge, a DC corona discharge, and a plasma jet 21 sparged the off-gas of a packed-bed dielectric barrier 22 Of <sup>23</sup> discharge (PB-DBD).  $H_2O_2$ ,  $NO_2^-$ , and  $NO_3^-$  are produced <sup>24</sup> after plasma exposure and only NO<sub>3</sub><sup>-</sup> after off-gas sparging. 25 Short-lifetime species in plasma such as OH radicals act as <sup>26</sup> the precursors of  $H_2O_2$  and  $NO_2^-$ , and long-lifetime species 27 including N<sub>2</sub>O<sub>5</sub> act as the precursor of NO<sub>3</sub><sup>-</sup>. NO<sub>x</sub> may <sup>28</sup> inhibit  $H_2O_2$  production through OH consumption to produce <sup>29</sup> HNO<sub>2</sub> and HNO<sub>3</sub>. O<sub>3</sub> is found not to be the precursor of 30 ROS/RNS. In this work, the highest production efficiencies  $_{31}$  of H<sub>2</sub>O<sub>2</sub> and NO<sub>2</sub><sup>-</sup> are obtained to be 31.2 and 5.0  $\mu$ mol/kJ,  $_{32}$  respectively, by pulsed-plasma exposure, and that of NO<sub>3</sub><sup>-</sup> is 33 obtained to be 11.3 µmol/kJ by the off-gas sparging of the 34 PB-DBD.

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